TSEK03: Radio Frequency Integrated Circuits (RFIC)

Lecture 2: Noise

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Overview

- Razavi: Chapter 2.3, pp. 35-58.

- Lee: Chapter 11, pp. 334-362.

- Noise: Sources of noise, noise spectrum, thermal noise, 1/f (flicker) noise.

- Calculations: Noise in circuits and noise calculation, noise factor/figure, Friis' equation for cascaded noisy circuits blocks.

Flicker Noise

- Flicker noise or 1/f noise appears at low frequencies. It increases when frequency decreases.

- Flicker noise in MOSFET

$$\overline{V_n^2} = \frac{K}{WLC_{ox}}\frac{1}{f}$$
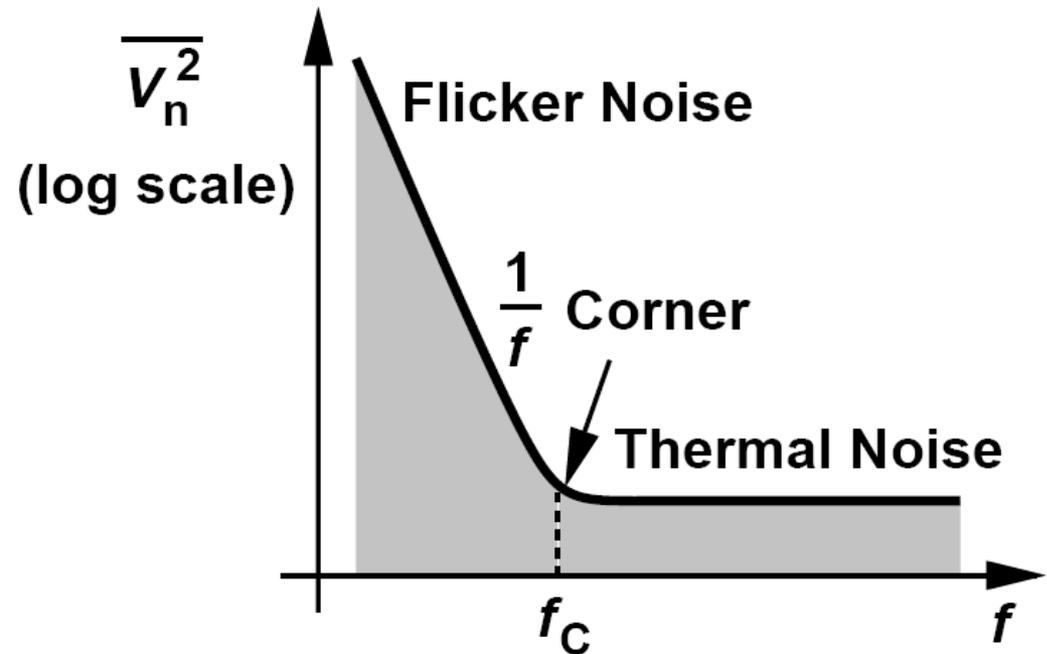
Transistor width   Gate length

- *K* is a process dependent constant, which is typically lower for PMOS devices than NMOS transistors.

Flicker Noise: corner frequency

$$\overline{V_n^2} = \frac{K}{WLC_{ox}}\frac{1}{f}$$

$$\frac{K}{WLC_{ox}}\frac{1}{f_c}g_m^2 = 4kT\gamma g_m$$

$$f_c = \frac{K}{WLC_{ox}}\frac{g_m}{4kT\gamma}$$

$\overline{V_n^2}$

(log scale)

Flicker Noise

$\frac{1}{f}$ **Corner**

Thermal Noise

f_C

f

- For CMOS devices, the 1/f noise corner falls in the range of tens or hundreds of MHz in today's MOS technologies.

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Noise in Bipolar Transistors

- Bipolar transistors contain physical resistances in their base, emitter, and collector regions, all of which generate thermal noise. Moreover, they also suffer from "shot noise" associated with the transport of carriers across the base-emitter junction.

- In low-noise bipolar circuits, the <u>base resistance thermal noise</u> and the <u>collector current shot noise</u> become dominant. For this reason, wide transistors biased at high current levels are employed.
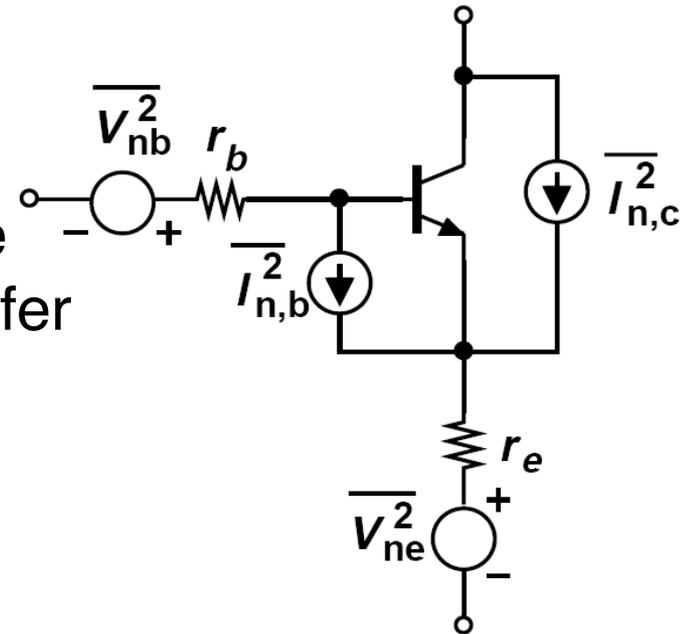
Noise Temperature

- Sometime you can see the term "Noise Temperature". What is this?

- Definition: "the equivalent temperature of a source impedance into a perfect (noise-free) device that would produce the same added noise".

$$F = 1 + \frac{T_N}{T_{ref}} \Rightarrow T_N = T_{ref}(F - 1) \qquad T_{ref} = 290 \text{ K}$$

- Ex:
  NF=3 dB => T_N = 289 K
  NF=1 dB T_N = 75 K

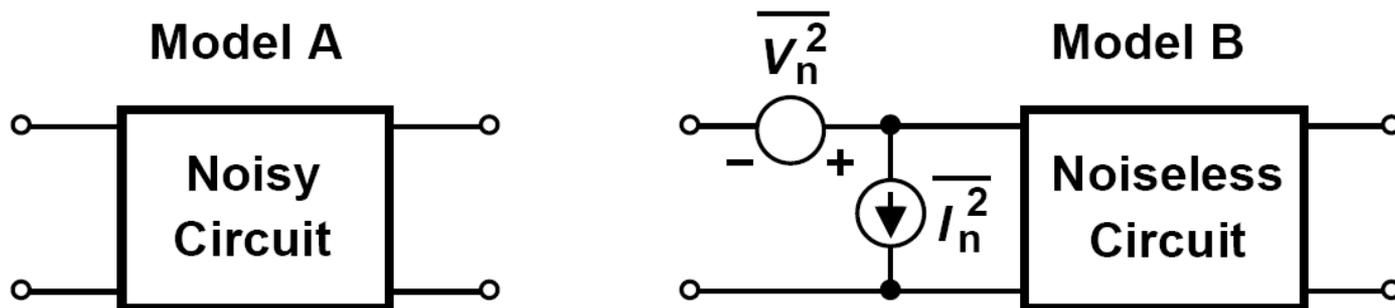# 2.3.5 Representation of noise in circuits

- All noise sources inside a circuit can be referred to its input, <u>input-referred noise</u>. The reason is that to disregard the effect of the gain on the circuit noise.

- Modeled by a series voltage source and a parallel current source:
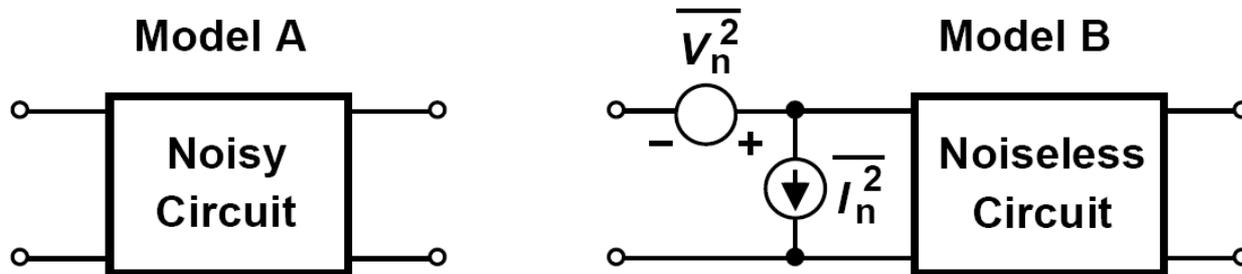
- These sources are assumed to be correlated.

Input-referred noise

- Voltage source: short the input port of models A and B and equate their output noise voltage (dividing the output noise by the voltage gain).

- Current source: leave the input ports open and equate the output noise voltage (dividing the output noise by the transimpedance gain).
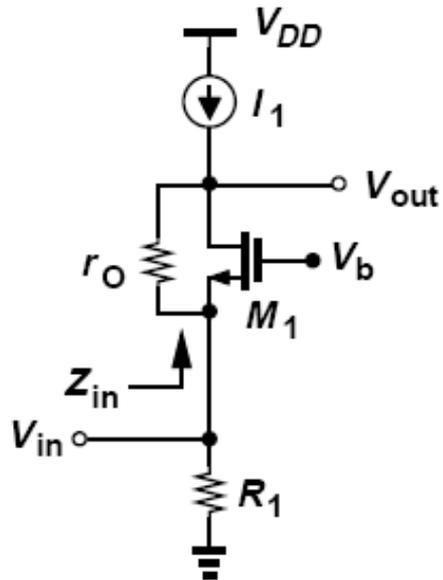
Model A

Noisy Circuit

$\overline{V_n^2}$

Model B

$\overline{I_n^2}$

Noiseless Circuit

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Example 2.18

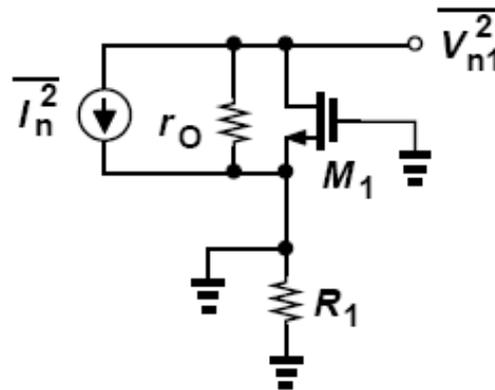- Calculate the input-referred noise of the common-gate stage depicted in figure below (left). Assume I_1 is ideal and neglect the noise of R_1.

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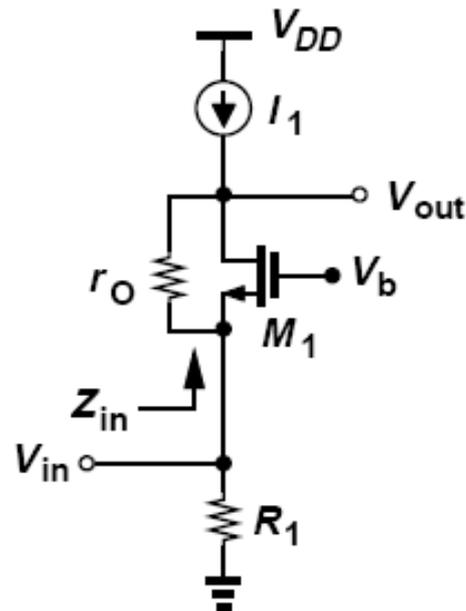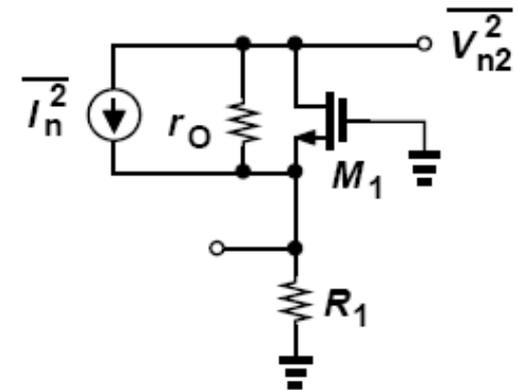
Example 2.18 (cont)

(a) CG stage

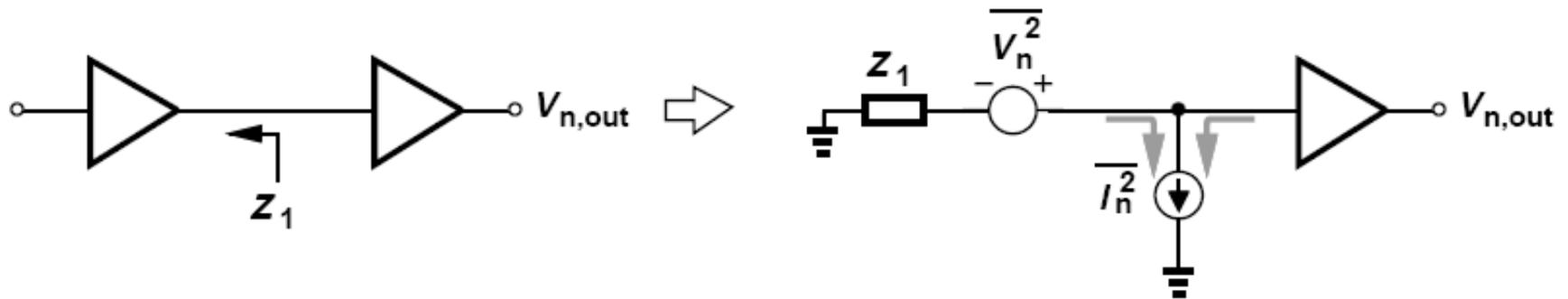(b) computation of input-referred noise voltage

(c) computation of input-referred noise current

Example 2.19

- Explain why the output noise of a circuit depends on the output impedance of the preceding stage.

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Example 2.19

- Explain why the output noise of a circuit depends on the output impedance of the preceding stage.

Noise Figure/Factor

- Noise figure (factor) shows the noise performance of a system.

$$NF = \frac{SNR_{in}}{SNR_{out}}$$ Noise Factor

- It can be expressed in dB:

$$NF\Big|_{dB} = 10\log\frac{SNR_{in}}{SNR_{out}}$$ Noise Figure

- NF depends on not only the noise of the circuit under consideration but the SNR provided by the preceding stage.

- If ideally a system adds no noise, F=1.

- If the input signal contains no noise, NF=∞.
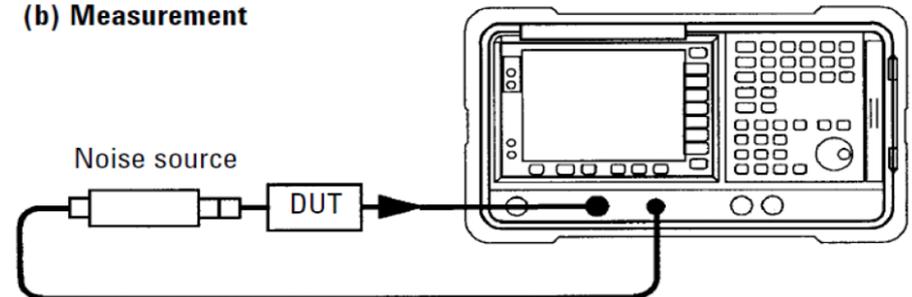
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NF measurements

- A noise source is used to create a controlled noise level.

- Avalanche diode in reverse mode is commonly used.

- OFF: noise temp=290 K
  ON: noise temp=10 000 K

(a) Calibration

Noise source

Measurement reference plane

(b) Measurement

Noise source
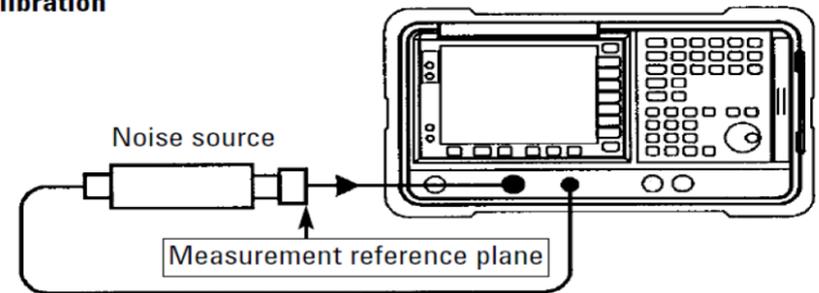
DUT
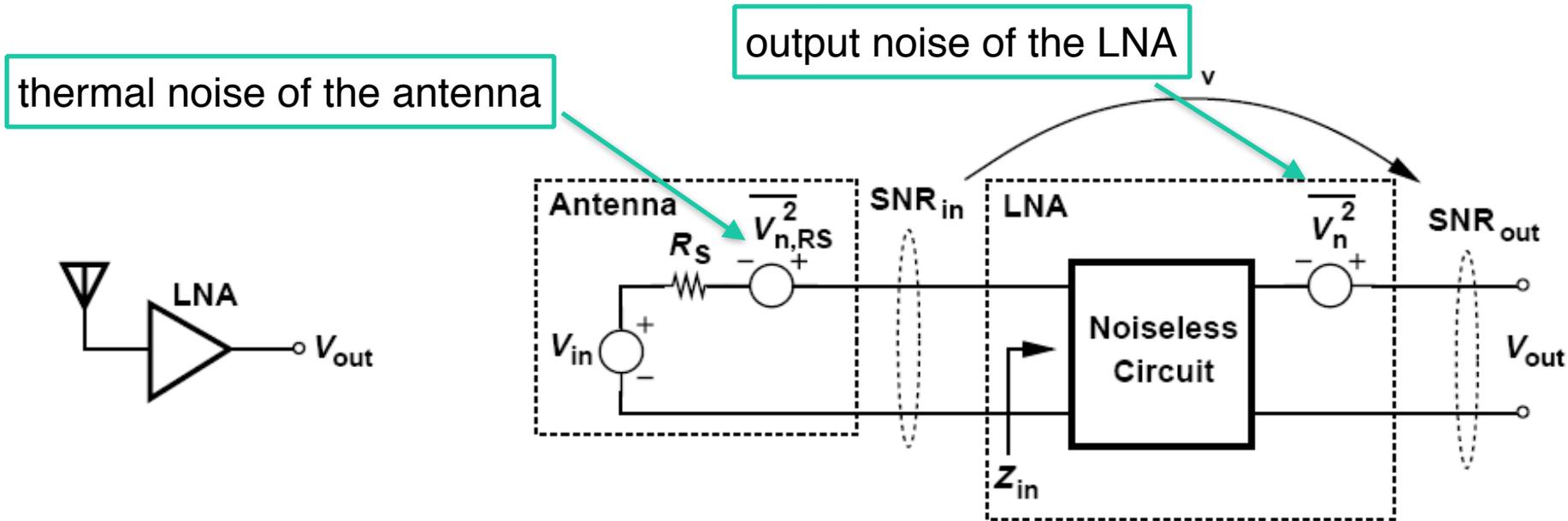
read more at:
Course page/Course documents/Additional readings

Calculation of Noise Figure

- Example: Low-noise amplifier (LNA) sensing the signal received by an antenna. NF of the LNA?

- Antenna "radiation resistance", R_S, produces noise.
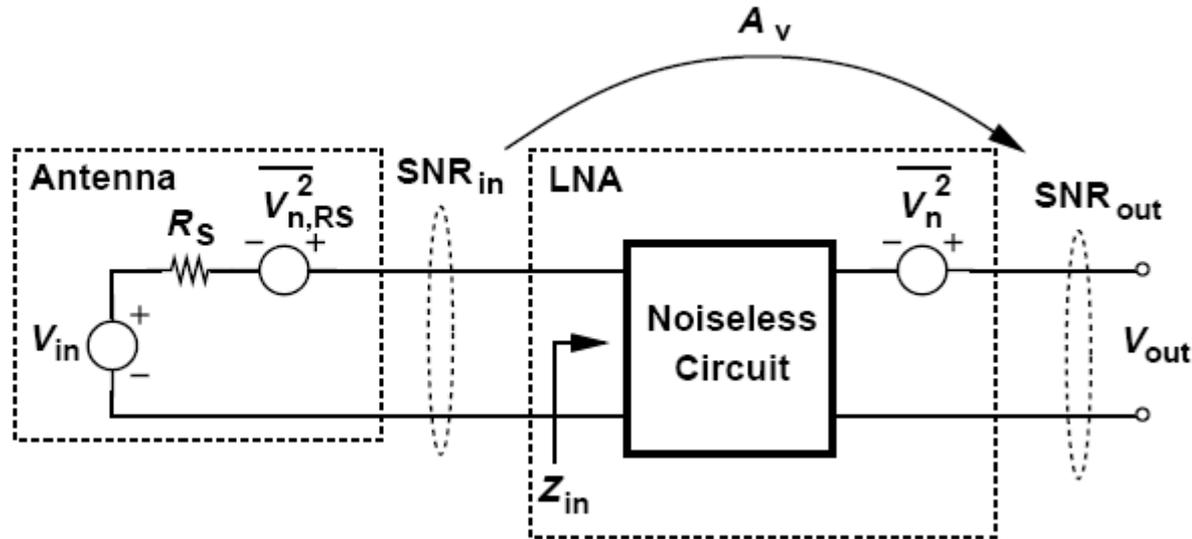
- Compute SNRin at the LNA input and SNRout at the output.

thermal noise of the antenna

output noise of the LNA

Noise Figure: SNR_{in}

- If LNA has Z_{in}, V_{in} and $V^2_{n,RS}$ are attenuated with
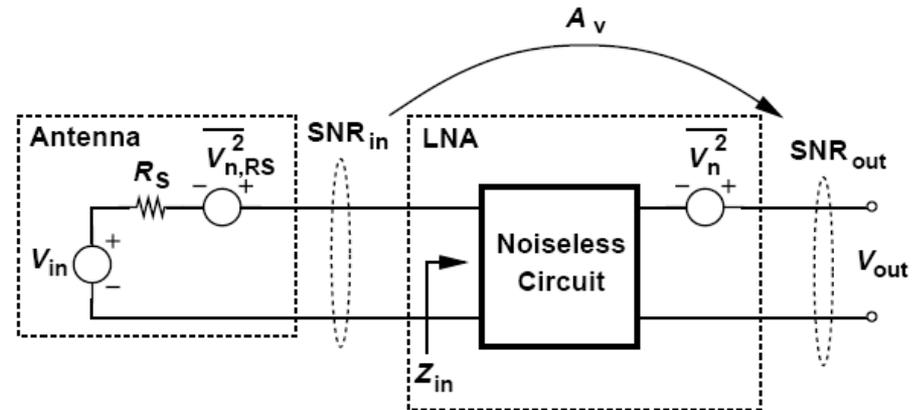 $α = Z_{in}/(Z_{in} + R_S)$

$$SNR_{in} = \frac{|\alpha|^2 V_{in}^2}{|\alpha|^2 \overline{V_{RS}^2}}$$

Noise Figure: SNR$_{out}$

- Assume voltage gain A$_v$ over the LNA. Output signal power is $V_{in}^2 |\alpha|^2 A_v^2$

- Output noise (uncorrelated, can be added):
  (a) the noise of the antenna amplified by the LNA
  (b) the output noise of the LNA

$$SNR_{out} = \frac{V_{in}^2 |\alpha|^2 A_v^2}{\overline{V_{RS}^2}|\alpha|^2 A_v^2 + \overline{V_n^2}}$$

Noise Figure

$$SNR_{in} = \frac{|\alpha|^2 V_{in}^2}{|\alpha|^2 \overline{V_{RS}^2}}$$

$$
\begin{aligned}
\text{NF} \quad &= \quad \frac{V_{in}^2}{4kTR_S} \cdot \frac{\overline{V_{RS}^2}|\alpha|^2 A_v^2 + \overline{V_n^2}}{V_{in}^2 |\alpha|^2 A_v^2} \\
&= \quad \frac{1}{\overline{V_{RS}^2}} \cdot \frac{\overline{V_{RS}^2}|\alpha|^2 A_v^2 + \overline{V_n^2}}{|\alpha|^2 A_v^2} \qquad (2.114)
\end{aligned}
$$

$$SNR_{out} = \frac{V_{in}^2 |\alpha|^2 A_v^2}{\overline{V_{RS}^2}|\alpha|^2 A_v^2 + \overline{V_n^2}}$$

$$
= \quad 1 + \frac{\overline{V_n^2}}{|\alpha|^2 A_v^2} \cdot \frac{1}{\overline{V_{RS}^2}}. \qquad (2.115)
$$

$$\alpha = Z_{in}/(Z_{in} + R_S)$$
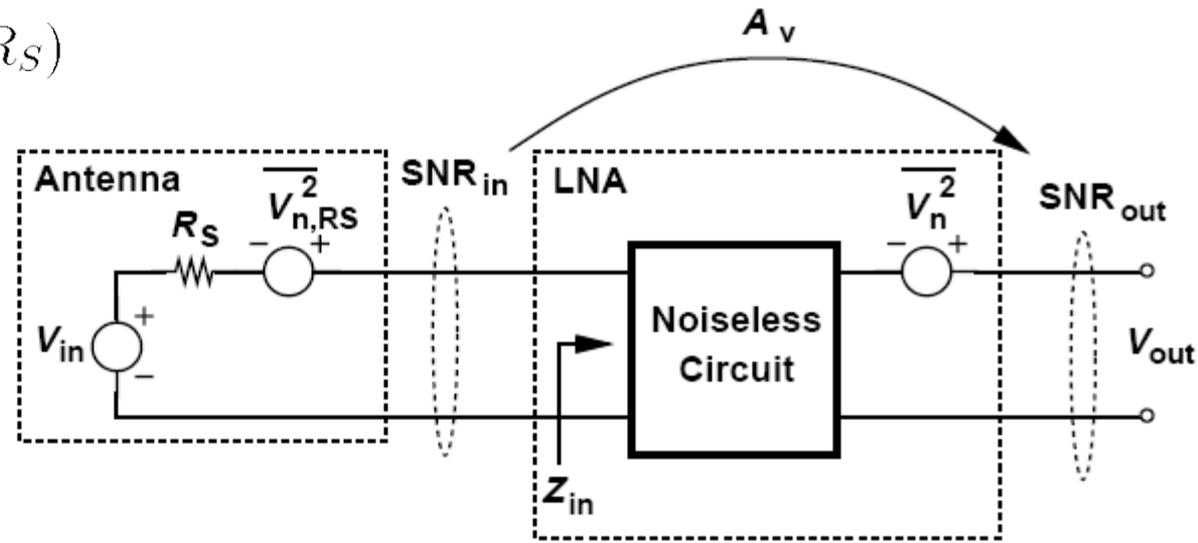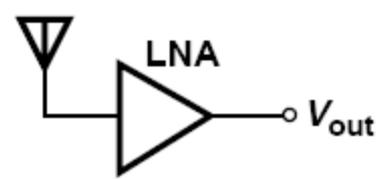
Noise Figure

- This results in a new definition for NF:
  NF= (total noise at the output) /
  (noise at the output due to the source impedance)

$$NF = \frac{\overline{V_{n,out}^2}}{A_0^2 \overline{V_{n,in}^2}}$$

- NF must be specified with respect to a source impedance, typically 50 Ω.

- Possible to reduce the right hand side of (2.114) to a simpler form:

$$\text{NF} = \frac{1}{4kTR_S} \cdot \frac{\overline{V_{n,out}^2}}{A_0^2} \qquad (2.116)$$

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Noise Figure Calculations

- Alt 1: Divide total output noise by the gain from V_{in} to V_{out} and normalize the result to the noise of R_s. (2.116)

- Alt 2: Calculate the output noise due to the amplifier, divide it by the gain, normalize it to $4kTR_s$ and add 1 to the result. (2.115)

- Valid even if no actual power is transferred, since they are based on voltage quantities.
  As long as the derivations incorporate noise and signal voltages, no inconsistency arises in the presence of impedance mismatches or even infinite input impedances.
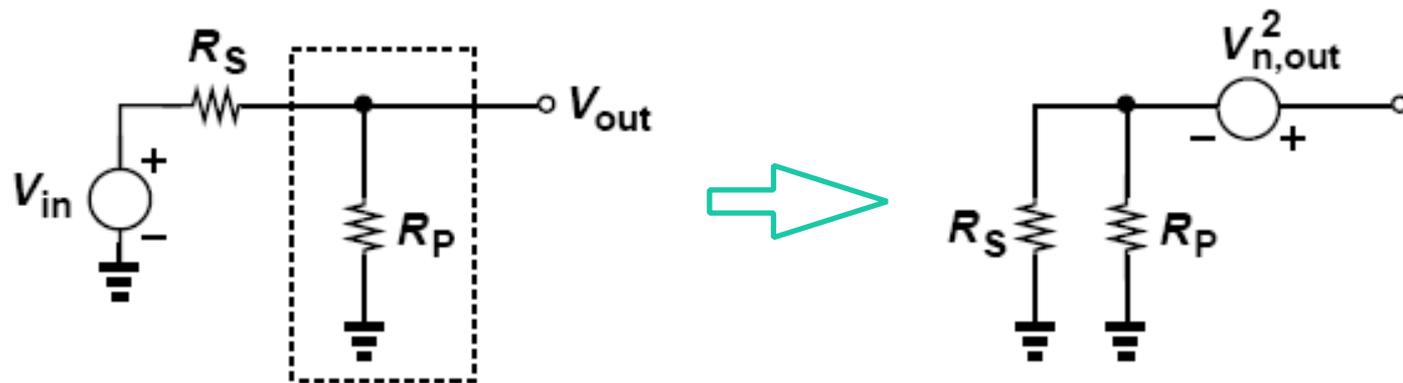
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Example 2.20

- Compute the noise figure of a shunt resistor R_P with respect to a source impedance R_S.
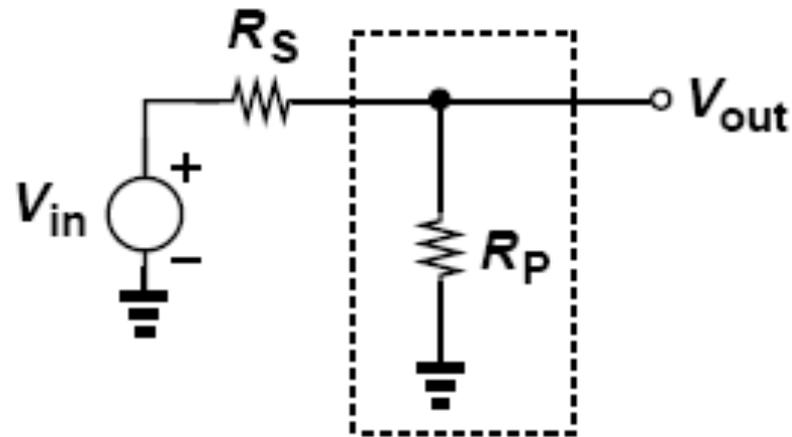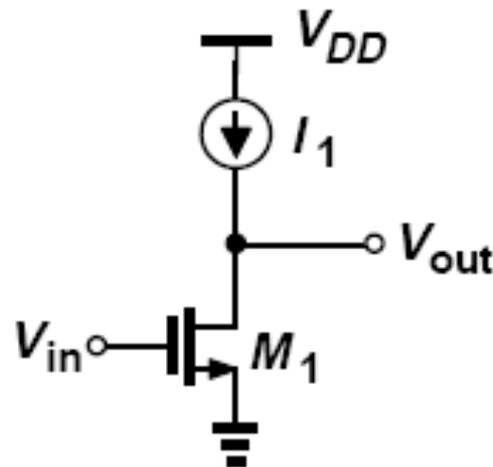
Example 2.20 (cont)

- Compute the noise figure of a shunt resistor R_P with respect to a source impedance R_S.

- Set V_{in} to zero and add a common noise source:

Example 2.21

- Determine the noise figure of the common-source stage shown in below with respect to a source impedance R_S. Neglect the capacitances and flicker noise of M_1 and assume I_1 is ideal.
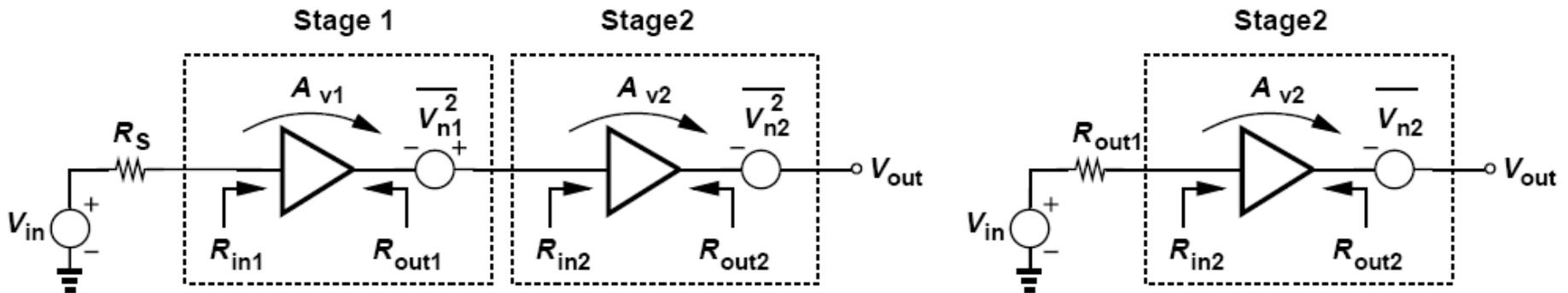
Example 2.21 (cont)

- Determine the noise figure of the common-source stage shown in below with respect to a source impedance R_S. Neglect the capacitances and flicker noise of M_1 and assume I_1 is ideal.
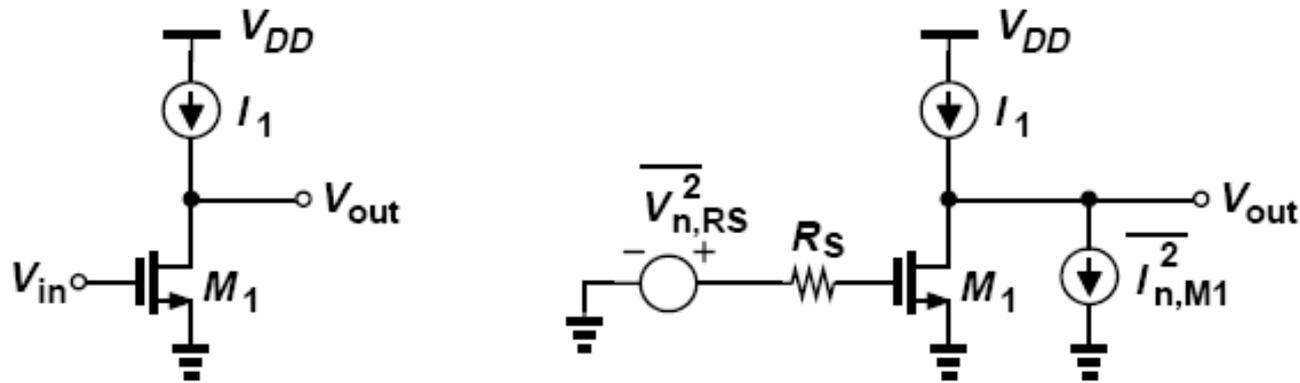
With added noise sources

Noise Figure of Cascaded Stages

$$NF_{tot} = 1 + (NF_1 - 1) + \frac{NF_2 - 1}{A_{P1}} + \cdots + \frac{NF_m - 1}{A_{P1} \cdots A_{P(m-1)}}$$

(2.132)

Gain is power gain, which depends on the impedance of each stage.

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Noise Figure of Cascaded Stages

- Simplified:

$$F_{sys} = F_1 + \frac{F_2 - 1}{G_1} + \frac{F_3 - 1}{G_1 G_2} + \dots \frac{F_n - 1}{G_1 G_2 \dots G_{n-1}}$$

- Called "Friis' equation": the noise contributed by each stage decreases as the total gain preceding that stage increases, implying that the first few stages in a cascade are the most critical.
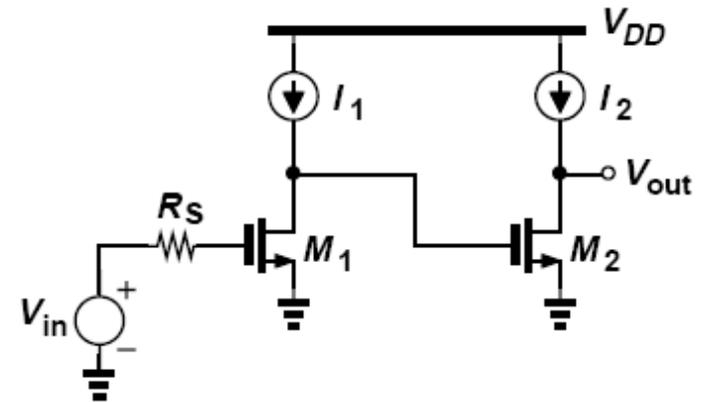
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Example 2.22

- Determine the NF of the cascade of common-source stages shown in figure below. Neglect the transistor capacitances and flicker noise.
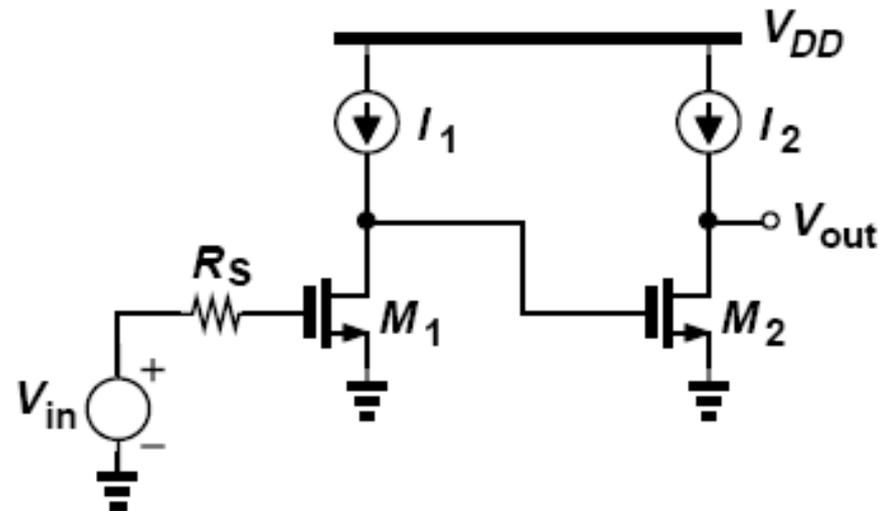
Example 2.22

$$R_{in1} \;=\; R_{in2} \;=\; \infty$$

$$NF = 1 + \frac{\overline{V_{n1}^2}}{A_{v1}^2}\frac{1}{4kTR_S} + \frac{\overline{V_{n2}^2}}{A_{v1}^2 A_{v2}^2}\frac{1}{4kTR_S}$$
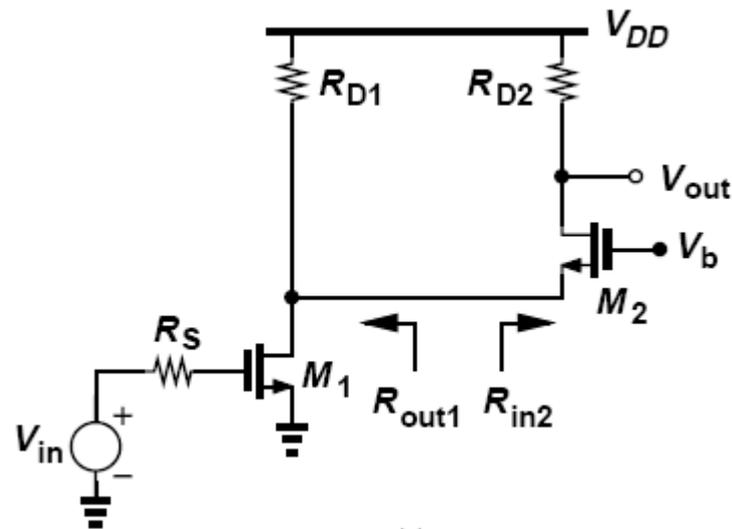
where

$$\overline{V_{n1}^2} = 4kT\gamma g_{m1} r_{O1}^2, \; \overline{V_{n2}^2} = 4kT\gamma g_{m2} r_{O2}^2, \; A_{v1} = g_{m1} r_{O1}, \text{ and } A_{v2} = g_{m2} r_{O2}.$$
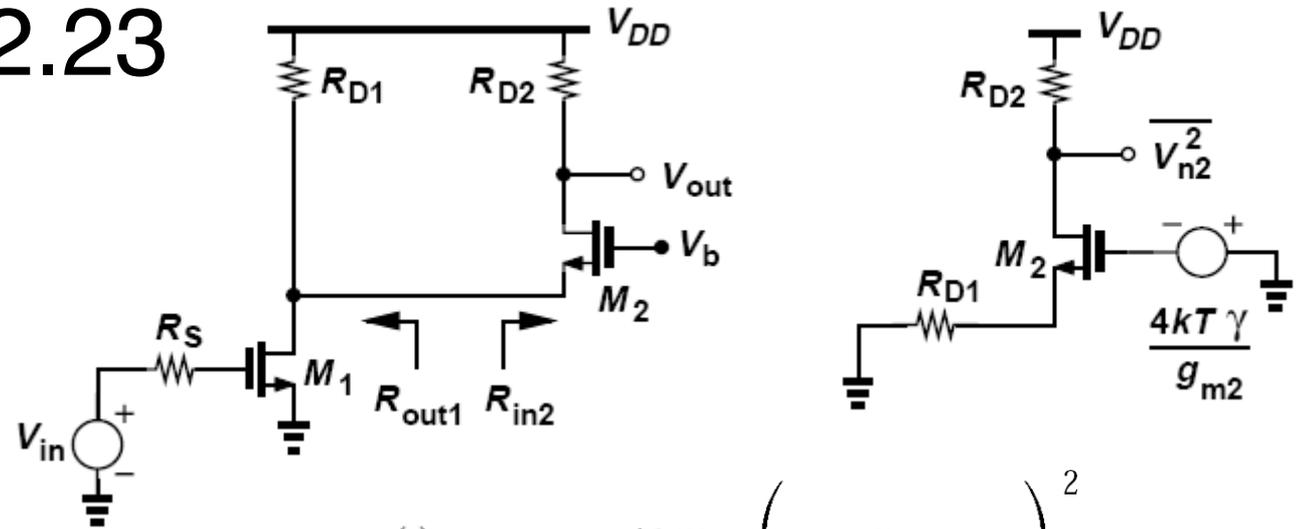
$$NF = 1 + \frac{\gamma}{g_{m1}R_S} + \frac{\gamma}{g_{m1}^2 r_{O1}^2 g_{m2} R_S}$$

Example 2.23

- Determine the noise figure of the circuit shown below. Neglect transistor capacitances, flicker noise, channel-length modulation, and body effect.
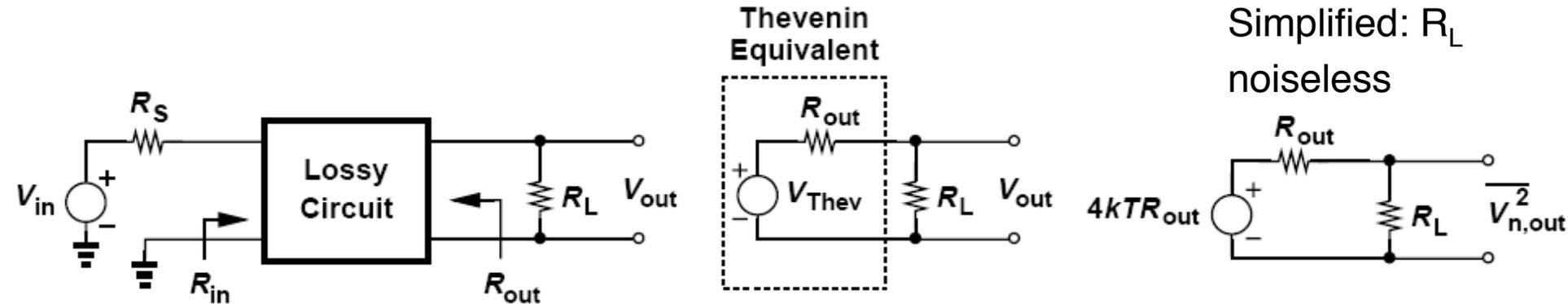
Example 2.23

$$\overline{V_{n1}^2} = 4kT\gamma g_{m1}R_{D1}^2 + 4kTR_{D1}$$

$$\overline{V_{n2}^2} = \frac{4kT\gamma}{g_{m2}}\left(\frac{R_{D2}}{\frac{1}{g_{m2}}+R_{D1}}\right)^2 + 4kTR_{D2}$$

$$NF_{tot} = 1 + \frac{4kT\gamma g_{m1}R_D^2 + 4kTR_{D1}}{g_{m1}^2R_{D1}^2}\cdot\frac{1}{4kTR_S}$$

$$+ \frac{\frac{4kT\gamma}{g_{m2}}\left(\frac{R_{D2}}{g_{m2}^{-1}+R_{D2}}\right)^2 + 4kTR_{D2}}{g_{m1}^2R_{D1}^2\left(\frac{g_{m2}^{-1}}{g_{m2}^{-1}+R_{D1}}\right)^2 g_{m2}^2R_{D2}^2}\cdot\frac{1}{4kTR_S}$$

Noise Figure of Lossy Circuits (pp. 56-58)

Thevenin Equivalent

Simplified: R_L noiseless

- Power loss (L):

$$L = P_{in}/P_{out}$$

$$\overline{V_{n,out}^2} = 4kTR_{out}\frac{R_L^2}{(R_L + R_{out})^2}$$

$$L = \frac{V_{in}^2}{V_{Thev}^2}\frac{R_{out}}{R_S}$$

$$A_0 = \frac{V_{Thev}}{V_{in}}\frac{R_L}{R_L + R_{out}}$$

$$NF = 4kTR_{out}\frac{V_{in}^2}{V_{Thev}^2}\frac{1}{4kTR_S}$$

$$= L.$$

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Example 2.24

- The receiver shown below incorporates a front-end band-pass filter (BPF) to suppress some of the interferers that may desensitize the LNA.
  If the filter has a loss of L and the LNA a noise figure of NF_{LNA}, calculate the overall noise figure.
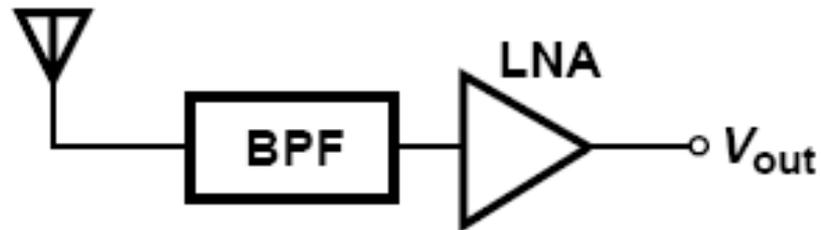
Summary, noise

- Noise is a random process

- Noise can be represented as sources using average squared values

- Noise has spectrum - Power Spectral Density PSD - and can be filtered

- Thermal noise = 4kTR

- MOSFETs: channel noise, gate noise, 1/f noise

- Circuit noise is usually represented by noise sources at the input: "input-referred noise"

- Noise figure and calculations

- Noise figures of cascaded stages: Friis' equation

- Noise of lossy circuits